

Smoothed particle hydrodynamics for fluid dynamics

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- Hw # 4: Finite difference method + MPI for Helmholtz equations

- If you need a multi-core machine: apply for a CCV account
<https://www.ccv.brown.edu/>

Outline

- 1 Background
 - hydrodynamic equations
 - numerical methods
- 2 Mathematics of smoothed particle hydrodynamics
 - some facts and basic mathematics
 - kernel and particle approximations of a function
 - first and second derivatives
- 3 Particles for hydrodynamics
 - continuity and pressure force
 - viscous force
- 4 Classical mechanics for particles \Rightarrow hydrodynamics
 - density estimate
 - equations of motion
- 5 Numerical errors
- 6 Research challenges
- 7 A short excursion to other particle methods

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Total mass flows out of the volume V (per unit time) by surface integral

$$\oint \rho \mathbf{v} \cdot d\mathbf{f}, \quad (1)$$

where ρ density, \mathbf{v} velocity and $d\mathbf{f}$ is along the outward normal.
The decrease of the mass in the volume (per unit time)

$$-\frac{\partial}{\partial t} \int \rho dV. \quad (2)$$

For a mass conservation, we have an equality

$$-\frac{\partial}{\partial t} \int \rho dV = \oint \rho \mathbf{v} \cdot d\mathbf{f} = \int \nabla \cdot (\rho \mathbf{v}) dV, \quad (3)$$

which is valid for an arbitrary V . The continuity equation reads

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0. \quad (4)$$

Total pressure force acting on the volume (surface to volume integral)

$$-\oint p d\mathbf{f} = -\int \nabla p dV. \quad (5)$$

For a *unit* of volume, momentum equations in Lagrangian form read

$$\rho \frac{d\mathbf{v}}{dt} = -\nabla p \quad \text{or} \quad \frac{d\mathbf{v}}{dt} = -\frac{\nabla p}{\rho}. \quad (6)$$

Considering the particle derivative is related to the partial derivatives as

$$\frac{d}{dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla, \quad (7)$$

the Euler equations in Eulerian form read

$$\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} = -\frac{\nabla p}{\rho}. \quad (8)$$

For real fluids, we need to add in viscous stress due to irreversible process and assume that the viscous stress depends only *linearly* on derivatives of velocity.

Without derivation, the Navier-Stokes equations read

$$\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} = -\frac{1}{\rho} [\nabla p + \eta \Delta \mathbf{v} + (\zeta + \eta/3) \nabla \nabla \cdot \mathbf{v}] \quad (9)$$

For an incompressible fluid $\rho = \text{const.}$ and $\nabla \cdot \mathbf{v} = 0$.

Therefore, the momentum equations simplify to

$$\frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \cdot \nabla \mathbf{v} = -\frac{1}{\rho} (\nabla p + \eta \Delta \mathbf{v}). \quad (10)$$

For a compressible fluid, an equation of state is called for

$$p = p(\rho, T = T_0). \quad (11)$$

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Prof. Karniadakis will cover the mesh-based methods in other lectures

- finite difference method
- spectral h/p element method
-

Mesh-free discretizations: mesh-free = mess-free?

- Some particle methods
 - smoothed particle hydrodynamics (SPH)
 - moving least square methods (MLS)
 - vortex method
 - Voronoi tessellation
 -
- mesh-free \approx mess-free
 - no mesh generation
 - Lagrangian, no $\mathbf{v} \cdot \nabla \mathbf{v}$
 - complex moving boundary
 - incorporation of new physics
 -

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Integral representation of a function

- It was invented in 1970s (**author?**) [12, 8].

Given a scalar function $f(r)$ of spatial coordinate r , its integral representation reads

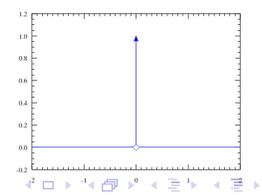
$$f(r) = \int f(r')\delta(r - r')dr', \tag{12}$$

where the Dirac delta function reads

$$\delta(r - r') \begin{cases} \infty, & r = r' \\ 0, & r \neq r' \end{cases} \tag{13}$$

and the constraint of normalization is

$$\int_{-\infty}^{\infty} \delta(r)dr = 1. \tag{14}$$



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SPH 1st step: smoothing or kernel approximation

(author?) [8]; (author?) [12]

Replace δ with another smoothly weighting function w :

$$f(r) \approx f_k(r) = \int f(r')w(r - r', h)dr', \tag{15}$$

where kernel w has properties

- 1 smoothness
- 2 compact with h as parameter
- 3 $\lim_{h \rightarrow 0} w(r - r', h) = \delta(r - r')$
- 4 $\int w(r - r', h)dr' = 1$
- 5 symmetric
- 6

Gaussian: $\frac{1}{a\sqrt{\pi}}e^{-r^2/a^2}$

compact: B-splines, Wendland functions ...

(author?) [15, 16, 19]

- a cubic function as reads ($h = 1$ for simplicity)

$$w(r) = \begin{cases} C_D(1-r)^3, & r < 1; \\ 0, & r \geq 1. \end{cases} \quad (16)$$

If we require the constraint of normalization in two dimension

$$\int_0^{2\pi} \int_0^1 C_2(1-r)^3 r dr d\theta = 1 \iff C_2 = \frac{10}{\pi} \quad (17)$$

- a piecewise quintic function reads

$$w(r) = C_D \begin{cases} (3-s)^5 - 6(2-s)^5 + 15(1-s)^5, & 0 \leq s < 1 \\ (3-s)^5 - 6(2-s)^5, & 1 \leq s < 2 \\ (3-s)^5, & 2 \leq s < 3 \\ 0, & s \geq 3, \end{cases} \quad (18)$$

where $s = 3r/h$ and $C_2 = 7/(478\pi h^2)$ and $C_3 = 1/(120\pi h^3)$.

- $f(r) = f_k(r) + error(h)$

Integral \iff summation

$$f_k(r) = \int f(r')w(r-r', h)dr' \quad (19)$$

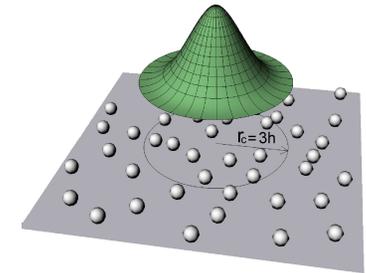
$$f_s(r) = \sum_i^{N_{neigh}} f_i w(r-r_i, h) V_i, \quad (20)$$

where V_i is a distance, area and volume in 1D, 2D, and 3D, respectively.

Therefore,

$$f_k(r) \approx f_s(r) \quad (21) \quad \text{summation within compact support}$$

- $f_k(r) = f_s(r) + error(\Delta r, h)$



An example: evaluation of density and arbitrary function

$\forall i$ of particle index, mass m_i , density ρ_i , and $V_i = m_i/\rho_i$.

$$f_s(r) = \sum_i^{N_{neigh}} f_i w(r-r_i, h) V_i = \sum_i^{N_{neigh}} \frac{m_i}{\rho_i} f_i w(r-r_i, h). \quad (22)$$

- What is the density at an arbitrary position r ?

$$\rho_s(r) = \sum_i^{N_{neigh}} \frac{m_i}{\rho_i} \rho_i w(r-r_i, h) = \sum_i^{N_{neigh}} m_i w(r-r_i, h). \quad (23)$$

- What is the density of a particle at r_j ?

$$\rho_s(r_j) = \sum_i^{N_{neigh}} m_i w(r_j-r_i, h). \quad (24)$$

- What is the value of a function of a particle at r_j ?

$$f_s(r_j) = \sum_i^{N_{neigh}} f_i \frac{m_i}{\rho_i} w(r_j-r_i, h) = \sum_i^{N_{neigh}} f_i W_{ji} = f_j \quad (25)$$

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$$f(\mathbf{r}) \approx f_k(\mathbf{r}) = \int f(\mathbf{r}') w(\mathbf{r} - \mathbf{r}', h) d\mathbf{r}' \quad (26)$$

$$\Downarrow$$

$$\nabla_r f(\mathbf{r}) \approx \nabla_r f_k(\mathbf{r}) = \nabla_r \int f(\mathbf{r}') w(\mathbf{r} - \mathbf{r}', h) d\mathbf{r}' \quad (27)$$

$$\Downarrow$$

$$\nabla_r f_k(\mathbf{r}) = \int \nabla_r f(\mathbf{r}') w(\mathbf{r} - \mathbf{r}', h) d\mathbf{r}' + \int f(\mathbf{r}') \nabla_r w(\mathbf{r} - \mathbf{r}', h) d\mathbf{r}' \quad (28)$$

$$\Downarrow$$

$$\nabla_r f_k(\mathbf{r}) = \int f(\mathbf{r}') \nabla_r w(\mathbf{r} - \mathbf{r}', h) d\mathbf{r}' \quad (29)$$

$$\Downarrow$$

$$\nabla_r f(\mathbf{r}) \approx \nabla_r f_k(\mathbf{r}) \approx \nabla_r f_s(\mathbf{r}) = \sum_i^{N_{neigh}} \frac{m_i}{\rho_i} f(\mathbf{r}') \nabla_r w(\mathbf{r} - \mathbf{r}', h) \quad (30)$$

$$\nabla_r \cdot f(\mathbf{r}) \approx \nabla_r \cdot f_k(\mathbf{r}) \approx \nabla_r \cdot f_s(\mathbf{r}) = \sum_i^{N_{neigh}} \frac{m_i}{\rho_i} f(\mathbf{r}') \cdot \nabla_r w(\mathbf{r} - \mathbf{r}', h) \quad (31)$$

$$\nabla_r \times f(\mathbf{r}) \approx \nabla_r \times f_k(\mathbf{r}) \approx \nabla_r \times f_s(\mathbf{r}) = \sum_i^{N_{neigh}} \frac{m_i}{\rho_i} f(\mathbf{r}') \times \nabla_r w(\mathbf{r} - \mathbf{r}', h) \quad (32)$$

Second derivatives

Note that we have following identity (**author?**) [4]

$$\int d\mathbf{r}' [f(\mathbf{r}') - f(\mathbf{r})] \frac{\partial w(|\mathbf{r}' - \mathbf{r}|)}{\partial r'} \frac{1}{r_{ij}} \mathbf{e}_{ij} \left[5 \frac{(\mathbf{r}' - \mathbf{r})^\alpha (\mathbf{r}' - \mathbf{r})^\beta}{(\mathbf{r}' - \mathbf{r})^2} - \delta^{\alpha\beta} \right]$$

$$= \nabla^\alpha \nabla^\beta f(\mathbf{r}) + \mathcal{O}(\nabla^4 f h^2). \quad (33)$$

Therefore,

$$\frac{1}{\rho_i} (\nabla^2 \mathbf{v}) = -2 \sum_j^{N_{neigh}} \frac{m_j}{\rho_i \rho_j} \frac{\partial w_{ij}}{\partial r} \mathbf{v}_{ij} \quad (34)$$

$$\frac{1}{\rho_i} (\nabla \nabla \cdot \mathbf{v}) = - \sum_j^{N_{neigh}} \frac{m_j}{\rho_i \rho_j} \frac{\partial w_{ij}}{\partial r} (5 \mathbf{e}_{ij} \cdot \mathbf{v}_{ij} \mathbf{e}_{ij} - \mathbf{v}_{ij}) \quad (35)$$

$$(36)$$

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- continuity equation is accounted for by

$$\rho_i = \sum_j^{N_{neigh}} m_j W_{ij}, \quad \dot{\mathbf{r}}_i = \mathbf{v}_i \tag{37}$$

- pressure force: $-\nabla p / \rho$

$$\mathbf{F}_i^C = \sum_j^{N_{neigh}} \mathbf{F}_{ij}^C = \sum_j^{N_{neigh}} -m_j \left(\frac{p_j}{\rho_j^2} \right) \frac{\partial w}{\partial r_{ij}} \mathbf{e}_{ij}, \tag{38}$$

- bad: not antisymmetric by swapping i and j
- recognize $-\nabla p / \rho = -\frac{p}{\rho^2} \nabla \rho - \nabla \frac{p}{\rho}$

$$\mathbf{F}_{ij}^C = -m_j \left(\frac{p_i}{\rho_i^2} + \frac{p_j}{\rho_j^2} \right) \frac{\partial w}{\partial r_{ij}} \mathbf{e}_{ij}, \tag{39}$$

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In general

$$\mathbf{F}_{ij}^D = \frac{m_j}{\rho_i \rho_j r_{ij}} \frac{\partial w}{\partial r_{ij}} \left[\left(\frac{5\eta}{3} - \zeta \right) \mathbf{v}_{ij} + \left(5\zeta + \frac{5\eta}{3} \right) \mathbf{e}_{ij} \cdot \mathbf{v}_{ij} \mathbf{e}_{ij} \right] \tag{40}$$

For inompression flows $\nabla \cdot \mathbf{v} = 0$, therefore,

$$\sum_j^N \frac{5}{\rho_i \rho_j r_{ij}} \frac{\partial w_{ij}}{\partial r_{ij}} \mathbf{e}_{ij} \cdot \mathbf{v}_{ij} \mathbf{e}_{ij} \approx \sum_j^N \frac{1}{\rho_i \rho_j r_{ij}} \frac{\partial w_{ij}}{\partial r_{ij}} \mathbf{e}_{ij}. \tag{41}$$

$$\mathbf{F}_{ij}^D = 2\eta \frac{m_j}{\rho_i \rho_j r_{ij}} \frac{\partial w_{ij}}{\partial r_{ij}} \mathbf{v}_{ij} \approx 10\eta \frac{m_j}{\rho_i \rho_j r_{ij}} \frac{\partial w_{ij}}{\partial r_{ij}} \mathbf{e}_{ij} \cdot \mathbf{v}_{ij} \mathbf{e}_{ij}. \tag{42}$$

Either choice is fine, but they are different.

- continuity equation:

$$\rho_i = \sum_j^{N_{neigh}} m_j W_{ij}, \quad \dot{\mathbf{r}}_i = \mathbf{v}_i \quad (43)$$

- momentum equations: (author?) [4, 11]

$$\dot{\mathbf{v}}_i = \sum_{j \neq i}^{N_{neigh}} (\mathbf{F}_{ij}^C + \mathbf{F}_{ij}^D), \quad (44)$$

$$\mathbf{F}_{ij}^C = -m_j \left(\frac{p_i}{\rho_i^2} + \frac{p_j}{\rho_j^2} \right) \frac{\partial w}{\partial r_{ij}} \mathbf{e}_{ij}, \quad (45)$$

$$\mathbf{F}_{ij}^D = \frac{m_j}{\rho_i \rho_j r_{ij}} \frac{\partial w}{\partial r_{ij}} \left[\left(\frac{5\eta}{3} - \zeta \right) \mathbf{v}_{ij} + \left(5\zeta + \frac{5\eta}{3} \right) \mathbf{e}_{ij} \cdot \mathbf{v}_{ij} \mathbf{e}_{ij} \right] \quad (46)$$

- weakly compressible: (author?) [2, 13]

$$p = c_T^2 \rho, \quad \text{or} \quad p = p_0 \left[\left(\frac{\rho}{\rho_r} \right)^\gamma - 1 \right] \quad (47)$$

p_0 relates to an artificial sound speed c_T

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Given a set of point particles with mass m_i , what is the density estimate for a position at r .

$$\rho_s(\mathbf{r}) = \sum_i^{N_{neigh}} m_i w(\mathbf{r} - \mathbf{r}_i, h). \quad (48)$$

where kernel w has properties

- smoothness
- compact with h as parameter
- $\int w(r - r', h) dr' = 1$
- symmetric
-

Eq. (48) is more fundamental than the summation form presented early

$$f_s(\mathbf{r}) = \sum_i^{N_{neigh}} f_i \frac{m_i}{\rho_i} w(\mathbf{r} - \mathbf{r}_i, h). \quad (49)$$

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Define the Lagrangian L as

$$L = T - U, \quad (50)$$

where T and U are kinetic and potential energies, respectively. For a set of particles

$$L = \sum_i^N m_i \left(\frac{1}{2} v_i^2 + u_i(\rho_i, s) \right) \quad (51)$$

Define the action as

$$S = \int L dt. \quad (52)$$

Minimizing S such that $\delta S = \int \delta L dt = 0$, where δ is a variation with respect to particle coordinate $\delta \mathbf{r}$. We have **(author?)** [17]

$$\delta S = \int \left(\frac{\partial L}{\partial \mathbf{v}} \cdot \delta \mathbf{v} + \frac{\partial L}{\partial \mathbf{r}} \cdot \delta \mathbf{r} \right) = 0 \quad (53)$$

$$\delta S = \int \left(\frac{\partial L}{\partial \mathbf{v}} \cdot \delta \mathbf{v} + \frac{\partial L}{\partial \mathbf{r}} \cdot \delta \mathbf{r} \right) = 0 \quad (54)$$

consider $\delta \mathbf{v} = d(\delta \mathbf{r})/dt$ and $d/dt = \partial/\partial t + \mathbf{v} \cdot \nabla$

\Downarrow

$$\delta S = \int \left\{ \left[-\frac{d}{dt} \left(\frac{\partial L}{\partial \mathbf{v}} \right) + \frac{\partial L}{\partial \mathbf{r}} \right] \cdot \delta \mathbf{r} \right\} dt + \left[\frac{\partial L}{\partial \mathbf{v}} \cdot \delta \mathbf{r} \right]_{t_0}^t = 0 \quad (55)$$

assume variation vanishes at start and end times and furthermore, $\delta \mathbf{r}$ is arbitrary. Therefore, we have the Euler-Lagrangian equations

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \mathbf{v}_i} \right) - \frac{\partial L}{\partial \mathbf{r}_i} = 0. \quad (56)$$

From the Lagrangian $L = \sum_i^N m_i \left(\frac{1}{2} v_i^2 + u_i \right)$ we know

$$\frac{\partial L}{\partial \mathbf{v}_i} = m_i \mathbf{v}_i, \quad \frac{\partial L}{\partial \mathbf{r}_i} = - \sum_j^{N_{neigh}} m_j \frac{\partial u_j}{\partial \rho_j} \frac{\partial \rho_j}{\partial \mathbf{r}_i} \quad (57)$$

Some basic thermodynamics: $dU = TdS - PdV$

Since $V = m/\rho$, so $dV = -md\rho/\rho^2$. For per unit mass we have

$$du = Tds - \frac{P}{\rho^2} d\rho. \quad (58)$$

For a reversible process $ds = 0$, therefore $\partial u_i / \partial \rho_i = p / \rho^2$. Put everything known into the Euler-Lagrangian equations, we get

$$\dot{\mathbf{v}}_i = \sum_{j \neq i}^{N_{neigh}} -m_j \left(\frac{p_i}{\rho_i^2} + \frac{p_j}{\rho_j^2} \right) \frac{\partial w}{\partial r_{ij}} \mathbf{e}_{ij}. \quad (59)$$

Euler hydrodynamics

- total mass $M = \sum_i^N m_i$.
- total linear momentum

$$\frac{d}{dt} \sum_i^N m_i \mathbf{v}_i = \sum_i^N m_i \frac{d\mathbf{v}_i}{dt} = \sum_i^N \sum_j^N -m_i m_j \left(\frac{p_i}{\rho_i^2} + \frac{p_j}{\rho_j^2} \right) \frac{\partial w}{\partial r_{ij}} \mathbf{e}_{ij} = 0. \quad (60)$$

- total angular momentum

$$\frac{d}{dt} \sum_i^N \mathbf{r}_i \times m_i \mathbf{v}_i = \sum_i^N m_i \left(\mathbf{r}_i \times \frac{d\mathbf{v}_i}{dt} \right) \quad (61)$$

$$= \sum_i^N \sum_j^N -m_i m_j \left(\frac{p_i}{\rho_i^2} + \frac{p_j}{\rho_j^2} \right) \frac{\partial w}{\partial r_{ij}} (\mathbf{r}_i \times \mathbf{e}_{ij}) = 0. \quad (62)$$

Similarly for the viscous forces.

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Errors in density estimate: kernel error

Recall the kernel approximation

$$\rho_k(\mathbf{r}) = \int \rho(\mathbf{r}') w(\mathbf{r} - \mathbf{r}', h) d\mathbf{r}', \quad (63)$$

Expanding $\rho(\mathbf{r}')$ by Taylor series around \mathbf{r}

$$\begin{aligned} \rho_k(\mathbf{r}) &= \rho(\mathbf{r}) \int w(\mathbf{r} - \mathbf{r}', h) d\mathbf{r}' + \nabla \rho(\mathbf{r}) \cdot \int (\mathbf{r}' - \mathbf{r}) w(\mathbf{r} - \mathbf{r}', h) d\mathbf{r}' \\ &+ \nabla^\alpha \nabla^\beta \rho(\mathbf{r}) \int \delta \mathbf{r}'^\alpha \delta \mathbf{r}'^\beta w(\mathbf{r} - \mathbf{r}', h) d\mathbf{r}' + O(h^3). \end{aligned} \quad (64)$$

Recall $\int w(\mathbf{r} - \mathbf{r}', h) d\mathbf{r}' = 1$ and odd terms vanish due to symmetric w ,

$$\rho(\mathbf{r}) = \rho_k(\mathbf{r}) + O(h^2). \quad (65)$$

Errors for a function f : kernel error and summation error

Similarly as for density estimate:

$$f(\mathbf{r}) = f_k(\mathbf{r}) + O(h^2). \quad (66)$$

Recall the particle approximation or summation form

$$f_k(\mathbf{r}_i) \approx f_s(\mathbf{r}_i) = \sum_j^{N_{neigh}} \frac{m_j}{\rho_j} f_j w(\mathbf{r}_i - \mathbf{r}_j, h). \quad (67)$$

Let us do Taylor series on $f(\mathbf{r}_j)$ around \mathbf{r}_i

$$f_s(\mathbf{r}_i) = f_i \sum_j^{N_{neigh}} \frac{m_j}{\rho_j} w(\mathbf{r}_{ij}, h) + \nabla f_i \cdot \sum_j^{N_{neigh}} \mathbf{r}_{ji} \frac{m_j}{\rho_j} w(\mathbf{r}_{ij}, h) + O(h^2). \quad (68)$$

To have error of $O(h^2)$, we need

$$\sum_j^N \frac{m_j}{\rho_j} w(\mathbf{r}_{ij}) = 1, \quad \sum_j^N \mathbf{r}_{ji} \frac{m_j}{\rho_j} w(\mathbf{r}_{ij}) = 0, \quad (69)$$

which is not guaranteed in practice (depends on configurations, Δx , and h).

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- 3 Particles for hydrodynamics
 - continuity and pressure force
 - viscous force
- 4 Classical mechanics for particles ⇒ hydrodynamics
 - density estimate
 - equations of motion
- 5 Numerical errors
- 6 **Research challenges**
- 7 A short excursion to other particle methods

- error analysis due to particle configurations
- consistency and conservation at the same time
- convergence for a practical purpose
- coarse-graining from molecular dynamics

- 1 Background
 - hydrodynamic equations
 - numerical methods
- 2 Mathematics of smoothed particle hydrodynamics
 - some facts and basic mathematics
 - kernel and particle approximations of a function
 - first and second derivatives
- 3 Particles for hydrodynamics
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- 6 **Research challenges**
- 7 **A short excursion to other particle methods**

- in a nutshell, \forall particle i in **SPH**, **SDPD**, **DPD**, or **MD**, the EoM:

$$\dot{\mathbf{v}}_i = \sum_{j \neq i} \left(\mathbf{F}_{ij}^C + \mathbf{F}_{ij}^D + \mathbf{F}_{ij}^R \right) \tag{70}$$

- options for different components
 - weighting kernel or potential gradient in MD
 - equation of state
 - density field
 - thermal fluctuations
 - canonical ensemble / NVT: thermostat
 -

SPH: (author?) [14]
 SDPD: (author?) [4]
 DPD: (author?) [10]; (author?) [5]; (author?) [9]
 MD: (author?) [1]; (author?) [7]; (author?) [6]; (author?) [18]

- ~ 12,000 SDPD particles (**author?**) [3]

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- hypnotized?

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